

A Comparison of RF Exposure in Macro- and Femtocells

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Abstract

This paper assesses radio frequency exposure of a mobile handset user in the context of a new class of cellular base station: the femtocell. Traditional cellular network construction relies on using a single base station to cover a large area and serve dozens to hundreds of users. The femtocell (named after the minuscule size of the coverage area) provides a low-power in-home cellular connection for the mobile handset. Consequently, we expect it to behave differently to a macrocell in terms of the users radio frequency energy exposure. Our work focuses on the trade-off in incident power on the mobile handset user when connected to either a macrocell or femtocell using power loss and power control models. Contrary to many individuals initial feeling that putting a base station in your home would increase exposure, our findings indicate that having a femtocell in the home will actual reduce the mobile handset users exposure to radio frequency energy.

I. INTRODUCTION

Cellular network providers have recently adopted a new method of dealing with the common problem of gaps in cellular network coverage: the femtocell. A femtocell is basically a compact, low power replica of the large mast-mounted wide- and local-area base stations (BSs) that are common to cellular systems. Femtocell base stations are designed to be deployed within the home and office environment. The purpose behind a femtocell is to provide the owner with a “5 bar” signal within the home, avoiding the need for a cellular subscriber to be serviced by the wide or local area base station. The network provider also benefits by offsetting a proportion of traffic to the subscriber’s broadband connection and by avoiding the installation of additional wide- and local-area base stations.

From the perspective of the cellular provider, these femtocells are a perfect solution to the long-running problem of signal penetration into complex structures (such as homes and offices). From the perspective of the home user, a femtocell will almost definitely improve their home coverage and signal fidelity. However, due to a common conception that wireless devices are

dangerous to individuals in close proximity (due to high transmit power levels), there is a public perception of risk in adding wireless base stations within the home [1].

There are two factors that run contrary to these fears. First, a femtocell base station is only permitted to transmit at a much lower power (125 mW for class 4 device [2]) compared to the mast-mount versions (> 20 W [3]). This is similar to the power of the ubiquitous wireless local area network (WLAN) access points (100 mW [2]). Second, the handset itself is a major contributor to the radio frequency (RF) exposure of the individual. Further, power control algorithms at both the handset and the femtocell base station may reduce the transmit power of both devices if the received signal level at each device warrants it.

In this paper, we look at the issue of femtocell RF exposure with an eye to the power control mechanism employed in the handset. We consider two mechanisms for RF exposure: from the base station (femto or macro) and from the handset. In modern handsets, a power control algorithm operates to minimize the transmit power in the hopes of maximising battery life. The signal loss between the base station and the handset is continually monitored and reported to the handset, which then adapts to maintain a certain desired received signal level at the base station.

Note that this paper focuses on the case where an individual will be using a cellular handset in the home, regardless of which base station they are connecting to.

II. CELLULAR NETWORKS

The original tenet of cellular communications as first formulated in the 1950's through 1970's [4] utilizes the concept of frequency reuse between distant cells. It relied on the basic physical premise of path loss (that the further away a transmitter is from a receiver, the lower the observed signal power) and that two equally sized cells can operate at the same frequency provided they are separated with a large enough distance.

Femtocell technology provides a modern extension to the original cellular concept. By apportioning a small sized "femto" cell within the larger macrocell network, the cellular provider can fill coverage gaps within a home and allow for a lower reuse factor (a factor that dictates how close same channel base stations can operate). While the deployment of femtocell has been a relatively painless process (multiple carriers throughout Europe and North America already have femto cell base stations on offer for the public), there are still open questions as to how such

systems will impact the cellular system as a whole. Particularly, interference between femtocells and macrocells are a hot research topic [5]–[8].

As a result of the introduction of femto cells, the issue of RF exposure has been raised [9], [10]. Our work looks at an interesting twist of using a femtocell within a home: that of reduced RF exposure. Current biological research studies are still looking for more data before making any decisions on the effects of low-level recurring RF exposure [11], but such academic endeavors do not stop individuals from being concerned over health issues of RF exposure. While the possibility that power may be reduced when the distance to the base station is small is known to the RF exposure community [2], we do not believe it has been studied in detail for femtocells.

III. CALCULATING RELATIVE EXPOSURE

The following section lays out an approach to calculating and contrasting the relative exposure of a cellular user in the home in the presence and absence of a femtocell. We begin by presenting the background and assumptions that we use throughout our calculations in III-A. Then we detail the radio frequency channel model that we use for path loss estimation in III-B. A discussion of RF exposure is given in Section III-C, followed by a summary of power control in the UMTS 3G cellular system in III-D. Finally, we introduce our RF exposure model in III-E, which integrates elements of the preceding sections.

A. Assumptions and System Parameters

In this work, we consider a femtocell deployed in an urban home environment in the European Universal Mobile Telecommunications System (UMTS) band (1.9-2.1 GHz). The assumption is that while a handset will have access to a macrocell base station throughout most of the home, there is a possibility that some areas will suffer from low or zero connectivity. Further, we assume that the handset is far enough from the macrocell base station to have a path loss exponent greater than 2; in [12], this distance was estimated to > 60 m, which is realistic for the majority of home scenarios.

For simplicity, we consider an isolated system, where there is a single handset plus the femtocell and macrocell base stations. Thus, we do not consider the effect of neighbouring femtocell, macrocell, or handset interference in this study. As most current deployments of femtocells are based on the UMTS 3G standard, we use the power control algorithms common

to that technology. We also assume no path loss between the handset and the user, *i.e.* 100% of the energy emitted by the handset is absorbed by the user. This provides us with an upper bound, as obviously a lower proportion of transmit energy is absorbed (otherwise communications could not be established).

Throughout the rest of this document, the convention when discussing power levels will be that lower-case letter p will correspond to power measured in Watts, and upper-case letter P will correspond to decibels referenced to 1 mW (dBm), *i.e.* $P = 10 \log(p/1 \text{ mW})$. All other units will be defined as necessary.

B. Channel Models

RF propagation was extensively studied throughout the 1980's and 1990's. Numerous RF propagation models have resulted from this research. RF signals propagate by both direct path (line of sight), by refraction (around corners) and by reflection (depending on the material). Due to the complexity of the RF channel, empirical models are the tool of choice for systems research [12], [13], although ray-tracing and experimental measurements have been used in academic study [9], [14], [15]. The empirical models benefit from ease-of-use and generality, and so we use them in our work.

As discussed in [4], [16], there are a number of empirical models to choose from for the 1.9-2.1 GHz UMTS band. Since we are considering a domestic urban scenario, we chose to use the log-distance path loss model [17], [18]. Other more specialized models such as the popular COST 231 Hata model [19] and the ECC-33 model [16] are limited to receiver-transmitter separation distances to greater than 1 km.

The power law model is commonly used to estimate the median power loss due to distance from the transmitter [20]. In this model, the path loss is a function of the distance d between the transmitter and receiver and a path loss coefficient n , where

$$L(d, n) = 10n \log_{10}(d) + L(d_0), \quad (1)$$

and $L(d_0)$ is the path loss at a reference distance, usually 1 m. $L(d_0)$ is commonly calculated using the Friis transmission equation to be $L(d_0) = 20 \log_{10}(4\pi d_0/\lambda)$. For the 1.9 GHz UMTS band, this means $L(d_0) \approx 38$ dB.

We require modeling of both indoor and outdoor channels, both of which scenarios have been empirically studied with the log-distance model. For the outdoor channel that would categorize our macrocell BS to handset path, the path loss exponent was measured to be in the range of 2.58 to 2.69. These results are for an obstructed channel and depends on the height of the BS.

For the indoor channel, the path loss exponent n has been measured to range from 1.2 to 6.5 [17], depending on the building structure and materials. For our purposes, we use values of 2.2, 3.0, and 4.0 [4], [17].

C. Radio Frequency Exposure

The European Commission, the American National Standards Institute (ANSI) and the Institute of Electrical and Electronics Engineering (IEEE) have defined limits on the RF exposure for the general public [21], [22]. The limits are frequency dependent: for the 1.9 GHz cellular band, the limits are stated in terms of the specific absorption rate (SAR), averaged over a volume containing 10 g of tissue and over any 6 minute period [22]. The limit is measured in Watts per kilogram, and is set at 0.08 W/kg for the whole-body, 2 W/kg localized for the head and trunk, and 4 W/kg localized for the limbs. Strictly speaking, SAR is a measure of heat absorption over a specified region, after taking into account the electric conductivity (σ) and mass density (ρ) of the region. That is,

$$SAR = \int_{\mathbb{V}} \frac{\sigma E(r)}{\rho} dr, \quad (2)$$

where \mathbb{V} is the volume, $E(r)$ is the electric field in V/m , σ is the electric conductivity in S/m , ρ is the mass density in kg/m^3 , and SAR is measured in W/kg .

In our study, we don't measure the SAR directly, but approximate it with the received power at a distance from the transmitter. We effectively replace the user's body with an ideal omnidirectional antenna, removing the effect of tissue conductivity and mass. Although our model is simple, it does provide a means to compare arrival powers as a function of distance between the user and a BS. We do not require exact SAR metrics for our study, since we are interested in the relative received power at the users location. We are thus interested solely in Watts rather than Watts per kilogram.

P_{user} (dBm)	Power incident at the users location
$P_{UE,tx}$ (dBm)	Power transmitted from the handset
$P_{UE,max} = 21$ dBm	Maximum transmit power from a class 4 handset [23]
$P_{UE,min} = -50$ dBm	Minimum transmit power from a handset [23]
$P_{MBS,tx}$ (dBm)	Power transmitted from the macro base station
$P_{FBS,tx}$ (dBm)	Power transmitted from the femto base station
$P_{MBS,max} = 46$ dBm	Maximum transmit power from the macro base station [3]
$P_{FBS,max} = 20$ dBm	Maximum transmit power from the femto base station [24]
$P_{MBS,0} = -81$ dBm	Wanted signal mean power at a macro base station [24]
$P_{FBS,0} = -77$ dBm	Wanted signal mean power at a femto base station [24]
L dB	Path loss between the BS and UE
α	Proportion of time that a base station spends transmitting in the absence of any active connection
β	Proportion of time spent in an active call state

TABLE I
SUMMARY OF VARIABLES.

D. Power Control

To begin, a summary of all the variables used in the following sections is provided in Table I. From this point on, we resort to cellular vernacular and refer to the mobile handset as the user equipment (UE). The transmit power control (TPC) algorithm for UMTS systems is an integral part of operation, and our aim is to use it to calculate the transmit power of a handset. For instance, when multiple users are connected to a base station, it is essential to have the uplink signals (from the handset to the base station) arrive at similar power levels because of technical requirements of the code division multiple access (CDMA) protocol [25] used in UMTS systems. Further, to conserve battery power, a handset is optimized to transmit at the lowest level possible.

In UMTS, the TPC algorithm is dependent on whether the system is operating in frequency division duplex (FDD) or time division duplex (TDD) mode. For FDD, the TPC operates as a closed-loop system, which is required since the channel is not symmetric [26]. Briefly, the system operates with an inner-loop, to compensate for short term channel fluctuations, and an outer-loop, to compensate for longer term variations. The base station measures the received power from a handset, and provides feedback to the handset to either increase or decrease its

transmit power. This feedback serves to continuously adjust the power levels until the system converges to a satisfactory steady state. For TDD, the channel can be viewed as symmetric in both uplink and downlink, and therefore an open-loop power control approach can be used [27].

Next, we consider both the UMTS FDD and TDD TPC algorithms and show that after applying a few principled assumptions, they can be considered to be identical. First, consider that the outer-loop of the FDD TPC was designed to compensate for both shadowing (severe signal attenuation due to some large obstruction) and variable interference levels. We propose here that in a femtocell, the TPC algorithm can be simplified. Interferers will be largely absent within a domestic femtocell (*e.g.* imagine a low-power cell with only one or two handsets and the requisite control channels). Furthermore, shadowing will not be a problem, since a general in-home setting will consist of relatively low-loss walls. Hence, we assume that the outer loop will be largely inactive, and we can simplify the FDD TPC algorithm to consider only the inner loop.

The inner loop of the TPC algorithm focuses on the signal to interference and noise ratio (SINR). The measured SINR at the base station is

$$SINR_{est} = P_{UE,tx} - L_{UL} - IN_{BS}, \quad (3)$$

that is, the transmission power ($P_{UE,tx}$) less the path loss in the uplink channel (L_{UL}) and the interference plus noise power (IN_{BS}). Then when the power control algorithm converges, the handset transmit power is

$$P_{UE,tx}^{FDD} = SINR_{target} + L_{UL} + IN_{BS}. \quad (4)$$

Similarly, for TDD power control [28], we have

$$P_{UE,tx}^{TDD} = SINR_{target} + \gamma L_{UL} + (1 - \gamma)L_0 + IN_{BS} + C, \quad (5)$$

where $\gamma \in [0, 1]$ is a weighting parameter based on the quality of the L_{UL} estimates, L_0 is the measured mean path loss, and C is some higher layer constant value that depends on the type of channel in use. This expression is identical to our simplified FDD expression if we trust the path loss estimate ($\gamma = 1$) and set $C = 0$. Finally, if we substitute $SINR_{target} = P_0 - IN_{BS}$, where P_0 is the desired receive level (sensitivity) at the base station in dBm, and include a maximum and minimum transmit power of the handset, then we have for both TDD and FDD

$$P_{UE,tx} = \max(\min(P_{UE,max}, P_0 + L_{UL}), P_{UE,min}), \quad (6)$$

where $P_{UE,max}$ and $P_{UE,min}$ are the maximum and minimum transmit powers of the handset. Note that values of P_0 vary between femtocells and macrocells. We assume that the desired receive level remains fixed, although in general it will be dependent on the current modulation and coding level selected.

E. Model-based Approximation for RF Exposure

We suggest that the power incident on a cellular handset user can be broken down into the following parts. The average power incident on an individual, p_{user} , is dependent on:

- $p_{UE,tx}$ is the power transmitted by the UE,
- $p_{BS,tx}$ is the power transmitted by the BS to the UE,
- L_{BS} is the path loss between the BS and the UE,
- α is the overhead coefficient (for BS discovery, synchronisation, *etc.*), and
- β is the proportion of time spent in an active call.

The last two components have to do with the dynamics of call-specific transmissions and constant overhead BS radiation (*e.g.* pilot and synchronization channels). Then, for a connection with a macrocell base station (MBS),

$$p_{user}^{(macro)} = p_{UE,tx}^{(macro)} \beta + p_{MBS,tx} 10^{-L_{MBS}/10} (\alpha + \beta), \quad (7)$$

where the first term is the power incident from the UE to the user, the second term is the power incident from the MBS to the user, and L_{MBS} is the path loss between the MBS and the UE. Similarly, for a connection with a femtocell BS (FBS),

$$p_{user}^{(femto)} = p_{UE,tx}^{(femto)} \beta + p_{MBS,tx} 10^{-L^{(macro)}/10} \alpha + p_{FBS,tx} 10^{-L_{FBS}/10} (\alpha + \beta), \quad (8)$$

where the first term is the power incident from the UE to the user, the second term is the power incident from the MBS to the user with path loss L_{MBS} , and the third term is the power incident from the FBS to the user with path loss L_{FBS} . We include this second term since the MBS background radiation is present regardless of the presence of the femtocell. Finally, we make the assumption that $p_{BS,tx} = p_{BS,max}$, which provides an upper bound for our exposure estimates. This is justified by there being no mandatory requirement for the BS to respond to the TPC requests from a handset [26].

Using this model, we can find the distance from the BS that will minimize the total exposure p_{user} . That is, find $d_{min} = \operatorname{argmin}_d p_{user}(d)$. This works out to be

$$d_{min} = \sqrt[2n]{\frac{p_{BS,tx}(\alpha + \beta)10^{-7.65}}{p_{BS,0}\beta}}, \quad (9)$$

where the $10^{-7.65}$ term comes straight from the path loss expression. Calculation of d_{min} is the same for both MBS and FBS scenarios if we assume that the macrocell is far enough away that we can approximate it to be at a fixed distance D_m from the UE.

IV. RESULTS

Our goal is to compare the RF exposure of a mobile handset user with and without a femtocell in the home environment. The distance between the UE to the MBS is denoted as d_m , and the distance between the UE to the FBS is denoted as d_f .

In order to compare and contrast the effective RF exposure due to an active call and to the continuous background radiation emitted by a femtocell, we consider four scenarios as follows:

- 1) No femtocell present, 24 hour average
- 2) Femtocell present, 24 hour average
- 3) No femtocell present, 3.29 minute average
- 4) Femtocell present, 3.29 minutes average

The 3.29 minute average is based on the average duration of a single call [29]. For the 24 hour average, we take an indicative example and assume that there are 5 calls/day [30], each duration 3.29 minutes, so 16.45 minutes/day. For the 3.29 minute call, we assume that a call is active for the duration.

To generate the exposure curves for these scenarios, we parameterise the RF power exposure expressions in (7) and (8) on the distance to the active BS, d . The pathloss L_{BS} between the active BS and handset is modelled using (1), while the transmit power of the handset $p_{UE,tx}$ is from (6). The value of β depends on the scenario, while α and L_{MBS} (for the femtocell case) have values justified in Section IV-B.

A. Experiments

In order to verify the power control functionality of a commodity handset, we ran some experiments using a Nokia X6 using the Vodafone network in Ireland, in and out of the vicinity

Resolution Bandwidth	10 kHz
Video Bandwidth	30 kHz
Center Frequency	1.95 GHz
Scanning Bandwidth	20 MHz
Detector	RMS, max hold

TABLE II
SPECTRUM ANALYZER SETTINGS FOR ROHDE & SCHWARZ FSL6.

of a femtocell. The Vodafone 3G uplink channels are in the 1950 to 1965 MHz range [31]. For the femtocell experiment, we attached a patch antenna onto the back of the handset: while we acknowledge that this will not provide an accurate measure of the *true* RF transmit power, in the context of measurements at different locations and distances, it provides a good estimate of the power control functionality of the handset. The antenna was connected to a Rohde & Schwarz FSL-6 spectrum analyzer, with settings in Table II.

Fig. 1 shows the results of the transmission from the handset when connected to the FBS within the home. 10 measurements were taken at points from 1 m to 10 m: the measurements from 1 m to 8 m were done with a strong line-of-sight component. Using a simple least squares fit, the estimate for path loss coefficient n is found to be $\hat{n} = 3.15$. This value fits well within the expected range.

Fig. 2 shows the results of the transmission from the handset when connected to the MBS within an office. Since it is difficult to tell relative distance from the base station in this context, a number of measurement points were selected from around our office at the National University of Ireland Maynooth to demonstrate a range of signal strengths. Table III gives details of the measurement locations. Comparing to the results in Fig. 1, it is clear that the spread in the macrocell points is much larger (≈ 75 dB for macro and ≈ 45 dB for femto). This result stems from the construction of the cellular system: MBSs have larger dynamic ranges and lower sensitivity levels, and accordingly must deal with a more diverse channel than FBSs. We can thus conclude that the handset does implement power control with a wide range of powers, as we expect.

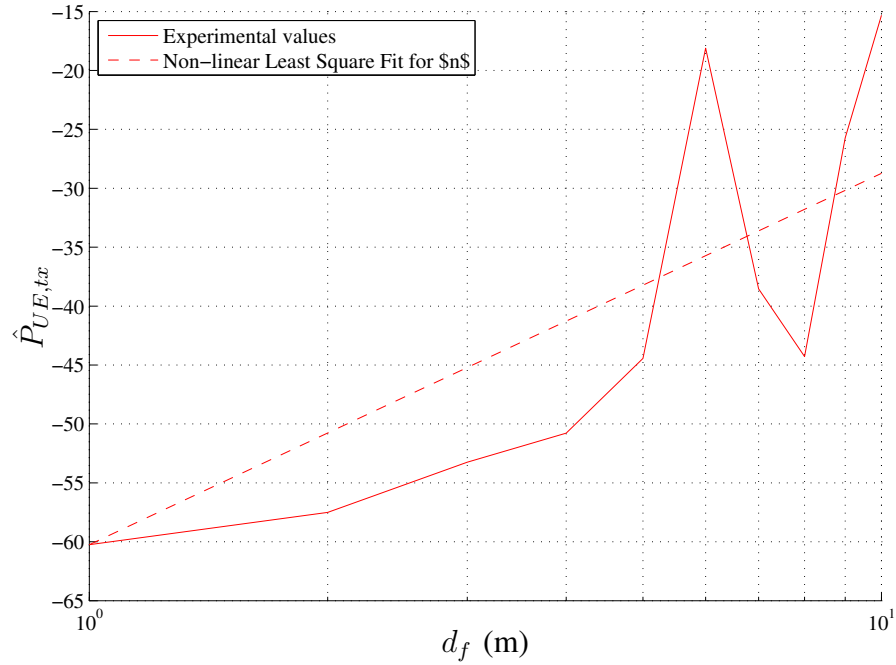


Fig. 1. Peak power values (RMS detector) versus distance for a femtocell connection. An estimate to the path loss exponent n is calculated using a non-linear least squares solver, and found to be $\hat{n} = 3.15$.

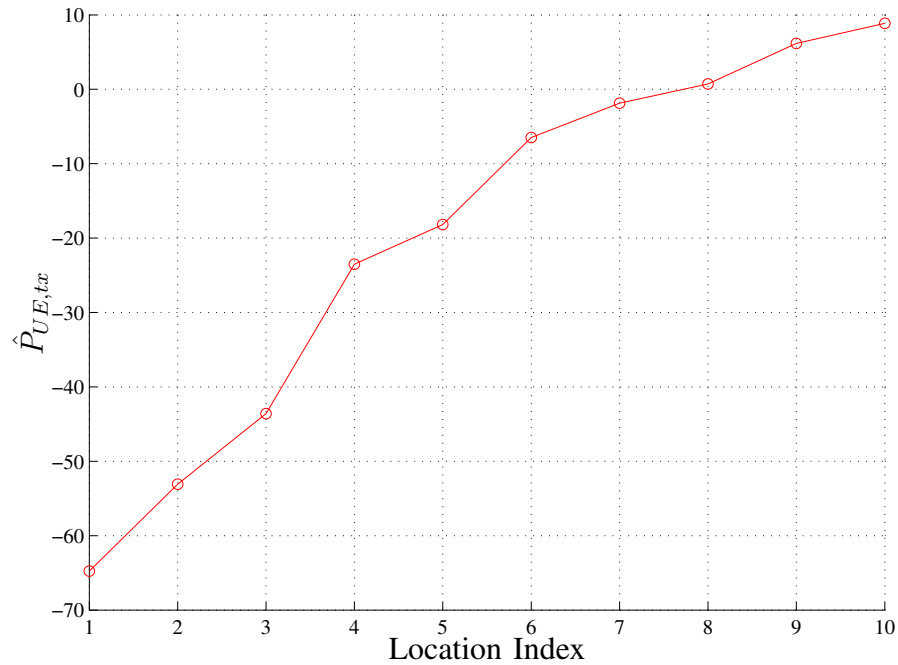


Fig. 2. Peak power values (RMS detector) versus location for a macrocell connection. Independent measurements are ordered in increasing measured transmit power. Table III provides the location cross-index.

1	In close proximity to a tree; handset situated on a tripod
2	On the front walk of an office; handset situated on a tripod
3	In office 1; handset situated on a tripod
4	In close proximity to a tree
5	On the front walk of an office
6	In office 1
7	In a hallway; handset situated on a tripod
8	In office 2; handset situated on a tripod
9	In a hallway
10	In office 2

TABLE III

MEASUREMENT LOCATIONS RELATING TO POINTS IN FIG. 2. NOTE THAT THERE ARE 5 INDEPENDENT MEASUREMENT LOCATIONS, EACH WITH TWO TYPES OF MEASUREMENT (THE HANDSET IS EITHER HELD IN HAND OR SITUATED ON A TRIPOD TO REMOVE ATTENUATION EFFECTS FROM THE HAND).

B. Simulations

With experimental results which confirm mobile handsets perform power control and have a wide range of transmit powers, we now use the model developed in Section III to explore relative RF exposure. Consider Figures 3 and 4, which show the power incident at a user averaged over a day or a call (3.29 minutes). The left hand graph in each figure shows incident power with a femtocell and the right hand without. We assume that $\alpha \approx 0.1$ on account of the common pilot channel (CPICH) and synchronization channel (SCH) [32]. Also, for the femtocell curves (dashed), the background radiation contribution from the MBS is approximated using $d_m = 100$ m. However, using our model, it is clear that the contribution $p_{BS,tx}^{(macro)}$ to the femtocell scenario is relatively inconsequential. Note that we see comparable results for the 6 minutes period required in SAR measurements, which a slight shift in the location of d_{min} and in the maximum exposure level when d is large.

The bold section of each curve corresponds to a typical range of distance from BS and UE, so $d_f \in [1, 50]$ m and $d_m \in [30, 1500]$ m. While the typical range for the FBS is based on its location in a room within a home, the MBS range is based on the physical constraints that i) the antenna is located on a mast or on a tall building, and ii) that the BS density will restrict the distance to a closer BS to less than a few kilometres in an urban setting. To verify this range, we

Location	Size of Sample Area (km ²)	Number of BSs in Sample Area	$\mathbb{E}[d_m]$ (m)	$\sqrt{\mathbb{E}[(d_m^2 - \mathbb{E}[d_m])^2]}$ (m)
North of Connolly Station	0.691	15	150.66	72.64
West of Lower Drumcondra Road	0.483	7	287.23	134.88
Donnybrook & Sandymount	9.661	58	320.73	206.70

TABLE IV

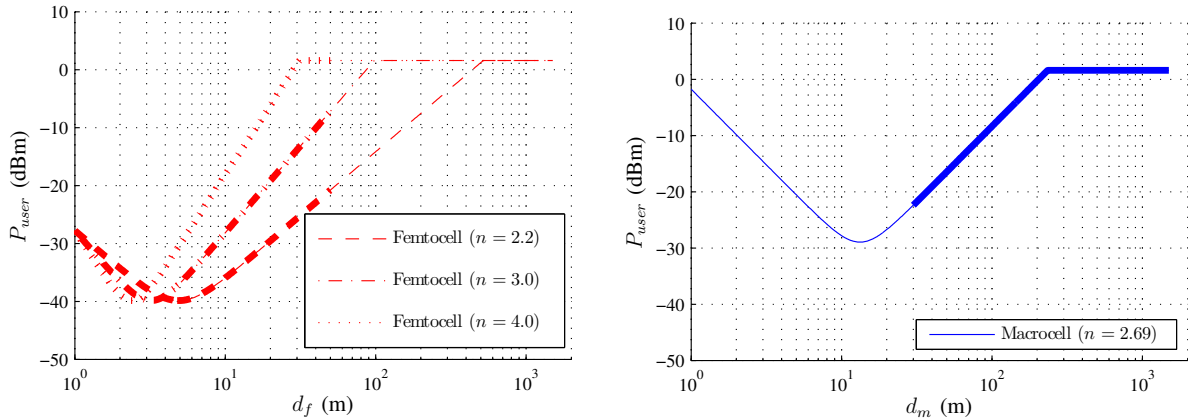
AVERAGE MINIMUM DISTANCE BETWEEN RANDOM LOCATIONS AND MBSs IN THREE DUBLIN RESIDENTIAL NEIGHBOURHOODS. BS LOCATIONS ARE BASED ON RECORDS FROM THE COMREG SITEVIEWER SERVICE [33]. SINCE THE LOCATIONS ARE GENERATED IN A UNIFORM RANDOM MANNER, THESE VALUES ARE INDICATIVE ONLY, AS INAPPROPRIATE LOCATIONS MAY BE USED IN THE AVERAGE (*i.e.* UNDERNEATH A BS MAST OR IN AN INACCESSIBLE AREA).

took samples of BS locations at specific geographic positions within residential areas of Dublin, Ireland, and then averaged over uniformly sampled random locations to find the average distance to the closest BS. The results indicate an average distance of 150 m to 300 m, with Table IV giving more detail.

For the 24 hour experiment, an individual at a distance $d_f < 15$ m from the FBS, assuming a path loss exponent $n < 3.0$, could expect an average exposure less than -23 dBm. If the same individual did not have a femtocell in their home, then in order to limit the exposure to the same level, they would need to be within a distance of approximately 30 m to a MBS. Since most macrocell sites are mast-mounted, this is a prohibitively close distance, and most users would most likely be in the hundreds of metres.

Comparing the experiment in Figure 3 and Figure 4, the most significant difference between the two plots is simply a vertical shift of the curves. This indicates that the contribution from the background RF energy amortized over a day proves to be small. There is a slight shift in the minimums to the left for the shorter experiment, on account of the lesser contribution from the base station to the average power.

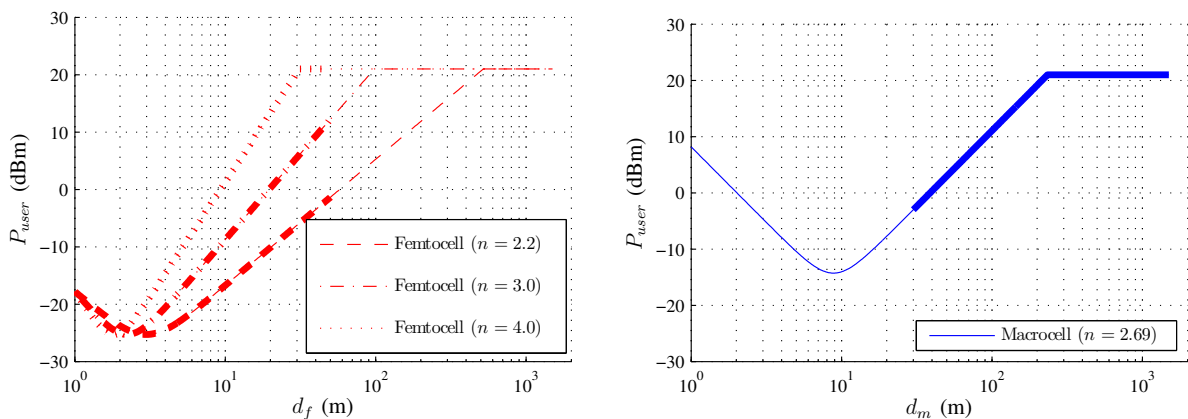
For the parameters shown, the minimum point d_0 from (9) is easily seen for all curves. For $d < d_{min}$, the dominant exposure mechanism is the macrocell/femtocell BS transmit power, while for $d > d_{min}$, it is the TPC of the UE. For the macrocell case, $d_{min}^{(macro)} = 13.62$ m for the 24 hour test and 9.07 m for the 3.29 minute test. The maximum $P_{user}^{(macro)}$ results from the MBS



(a) Femtocell exposure curves. Bold lines indicate the typical range: $[0, 50]$ m for femtocells.

(b) Macrocell exposure curves. Bold lines indicate the typical range: $[30, 1500]$ m for macrocells.

Fig. 3. Distance between BS and handset versus P_{user} . 24 hour average ($T = 24$ hours), UE connecting to femto or macro cell, 5 average length calls ($T_{UE} = 16.45$ minutes), $\beta = T_{UE}/T \approx 0.0114$.



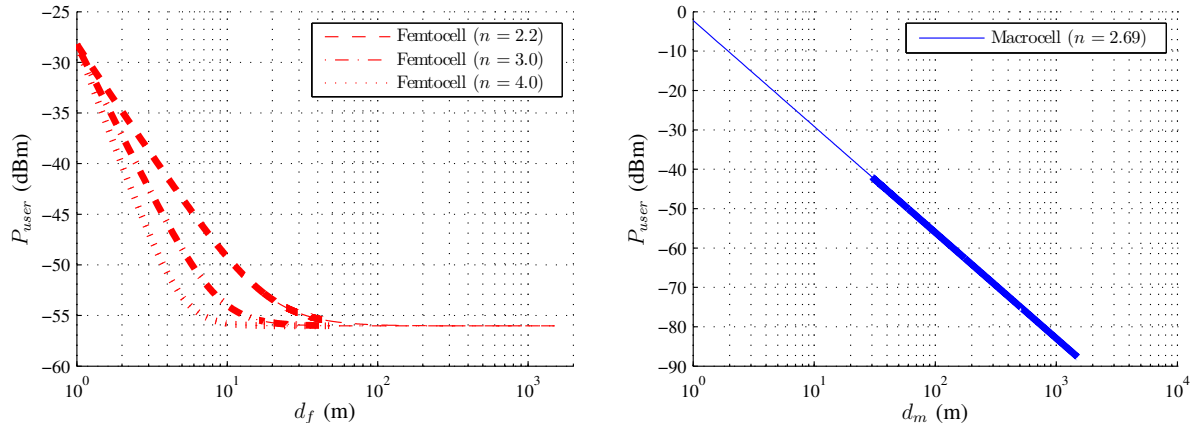
(a) Femtocell exposure curves. Bold lines indicate the typical range: $[0, 50]$ m for femtocells.

(b) Macrocell exposure curves. Bold lines indicate the typical range: $[30, 1500]$ m for macrocells.

Fig. 4. Distance between BS and handset versus P_{user} . 3.29 minute average ($T = 3.29$ minutes), UE connecting to femto or macro cell, UE transmitting constantly, call is in progress ($T_{UE} = 3.29$ minutes), $\beta = T_{UE}/T = 1$.

being far enough away from the UE that the UE TPC algorithm requires the maximum value, and is $P_{user}^{(macro)} \approx P_{UE,max} + 10 \log_{10} \beta$.

For the femtocell curves, we compare multiple path loss coefficients. The variation in d_{min} is a combination of all system components, as defined in (9). In general, by increasing the path loss coefficient, d_{min} will decrease. This corresponds to the UE needing to increase its transmit



(a) Femtocell exposure curves. Bold lines indicate the typical range: $[0, 50]$ m for femtocells.

(b) Macrocell exposure curves. Bold lines indicate the typical range: $[30, 1500]$ m for macrocells.

Fig. 5. Distance between BS and user versus P_{user} , in the absence of a UE, *i.e.* all traffic is background.

power to accommodate for the increased path loss. The location of the inflection point in effect defines the area where the exposure from the handset is minimised. For example, in the 24 hour test, the RF exposure is expected to be the same at a distance of 1 m of the FBS or at a distance of 5.5, 10 and 21 m, for $n = 4.0$, 3.0, and 2.2, respectively, with all points between having a lower RF exposure. Note that our model assumes that there is a minimum 38 dB attenuation between either BS and the UE, while for the handset there is no minimum attenuation. However, we consider this appropriate given that the UE will be located directly next to the users body, while the BS will always be at a distance of at least a few metres.

The last set of curves in Figure 5 look at RF exposure in the absence of a handset, *i.e.* all RF exposure is due to background radiation. As would be expected, RF exposure in the presence of a femtocell is much higher than without. The floor in the femtocell curves is due to the constant background macrocell contribution ($d_m = 100$ m). Compared to the previous figures, the RF exposure level is reduced when the individual is anywhere over d_{min} away from the BS.

V. DISCUSSION

Throughout this work, we have made a number of simplifying assumptions. These have allowed us to combine two relatively simple models, TPC and path loss, for the sake of estimating relative RF exposure levels. In summary, we have assumed that the TPC in UMTS systems is operating with a constant target, that the path loss will behave on average in a manner consistent

with the empirical models, and that the required receive sensitivity level is fixed. It is our view that these approximations do not detract from the comparison of femtocell scenario versus macrocell scenario, since each approximation is applied to each scenario.

In terms of the RF exposure, it is clear from the simulations that the maximum incident power or RF exposure is less in the case of the femtocell, primarily because of the smaller distance from the handset when compared to the macrocell and the similar target signal mean power (-81 dBm for the MBS and -77 dBm for the FBS).

For long-term exposure simulations (24 hour test), and considering typical separation distances between the handset and the BS, the femtocell scenario provides lower exposure if the user is standing less than 8 m away. This is true for any of the considered in-building fading scenarios.

When examining long-term exposure simulations (24 hour test), for typical separation distances we can consider when the femtocell scenario provides lower exposure than the *minimum* macrocell exposure. For our in-building scenarios with high path loss ($n = 4.0$), the femtocell provides lower exposure if the user is standing less than 8 m away. This range increases as the path loss decreases. As it could be expected that an individual would generally operate at a distance of a few metres from their in-building FBS, this shows that it should be expected that the individual would be subject to less RF exposure. For short-term exposure simulations (3 minute test), the same value of 8 m holds, with the difference being the location of the minimum exposure for both femtocell and macrocell scenario.

It should be kept in mind that the 8 m limit is chosen for the minimum incident power over the typical separation distances d_m in the macrocell case. This means a separation of 30 m between the user and BS. A more realistic value may be on the order of $d_m > 150$ m, in which case the incident power is close to saturation. The range of lower exposure when connected to a FBS will expand, *e.g.* for $d_m = 150$ m, the femtocell scenario provides lower exposure if the user is standing less than 20 m away.

To recast this exposure comparison in an everyday context, consider the following examples with more realistic sample values:

- 1) The owner of a small 10 X 15 m bungalow suffers from dropped calls as they move from their living room to their kitchen. They have checked with their service provider, and it appears that the nearest base station is 400 m away. Assuming a path loss coefficient of $n = 2.69$, their average RF exposure over the course of a day is estimated to be 21 dBm.

After installing a femtocell base station above the top of a bookshelf in their living room, the call drops have completely disappeared. Given the dimensions of the bungalow, the furthest from the femtocell BS the handset could be is 18 m. Assuming an indoor path loss coefficient of $n = 3$, the owners RF exposure has dropped to -1 dBm, a factor of over 150 times.

- 2) The owner of a large two-floor 20 X 20 m house has adequate cellular coverage throughout the home, but does notice some signal quality degradation when moving around the house. The nearest base station is only 150 m away. Assuming a path loss coefficient of $n = 2.69$, their average RF exposure over the course of a day is estimated to be 15.79 dBm. After installing a femtocell to improve their reception, with a path loss exponent of $n = 3.2$ and a floor height of 3 m (maximum separation from femtocell BS is then 28.44 m), the owners RF exposure has dropped to 7.75 dBm, a factor of over 6 times.

While the path loss coefficient n and its variation throughout a household will vary in a real-world situation, they are indicative of average values and are empirically-derived.

In this paper, we have presented a framework for gauging the relative benefit of new femtocell technology in terms of an individuals RF exposure. Our model is a combination of accepted empirical channel models and the standardised power control mechanism used in common-place cellular devices, which was explored via experimental results. In general, our results demonstrate that only in cases of excessive distance between the mobile user and the femtocell will the user experience more exposure than if connected to the macrocell.

In conclusion, this contribution is useful for system planners and groups that are seeking to minimize RF exposure. The expressions used to generate the simulated results are compact and easy-to-use, and only require an estimated path loss coefficient and the distances between the mobile user and the base station.

REFERENCES

- [1] W. H. Organization, "Electromagnetic fields and public health," Tech. Rep., <http://www.who.int/mediacentre/factsheets/fs304/en/index.html>.
- [2] The Int. Commission on Non-Ionizing Radiation Protection, *Health Physics*, vol. 94, no. 4, pp. 376–392, 2008, http://journals.lww.com/health-physics/Fulltext/2008/04000/Icnirp_Statement_on_Emf_Emitting_New_Technologies.11.aspx.
- [3] O. Arnold, F. Richter, G. Fettweis, and O. Blume, "Power consumption modeling of different base station types in heterogeneous cellular networks," in *Future Network and Mobile Summit*, Jun. 2010, pp. 1 –8.

- [4] T. S. Rappaport, *Wireless Communications: Principles and Practice*, Englewood Cliffs, NJ, 2006.
- [5] V. Chandrasekhar, J. Andrews, and A. Gatherer, "Femtocell networks: a survey," *IEEE Communications Magazine*, vol. 46, no. 9, pp. 59–67, Sep. 2008.
- [6] G. Jeney, "Practical Limits of Femtocells in a Realistic Environment," in *IEEE 73rd Vehicular Technology Conference (VTC)*, May 2011, pp. 1 –5.
- [7] V. Chandrasekhar and J. Andrews, "Uplink capacity and interference avoidance for two-tier femtocell networks," *IEEE Transactions on Wireless Communications*, vol. 8, no. 7, pp. 3498 –3509, Jul. 2009.
- [8] M. Yavuz, F. Meshkati, S. Nanda, A. Pokhariyal, N. Johnson, B. Raghothaman, and A. Richardson, "Interference management and performance analysis of UMTS/HSPA+ femtocells," *IEEE Communications Magazine*, vol. 47, no. 9, pp. 102 –109, Sep. 2009.
- [9] G. Koutitas and T. Samaras, "Exposure Minimization in Indoor Wireless Networks," *IEEE Antennas and Wireless Propagation Letters*, vol. 9, pp. 199 –202, 2010.
- [10] G. Korinthios, E. Theodoropoulou, N. Marouda, I. Mesogiti, E. Nikolitsa, and G. Lyberopoulos, "Early experiences and lessons learned from femtocells," *IEEE Communications Magazine*, vol. 47, no. 9, pp. 124 –130, Sep. 2009.
- [11] R. Baan, Y. Grosse, B. Lauby-Secretan, F. E. Ghisassani, V. Bouvard, L. Benbrahim-Tallaa, N. Guha, F. Islami, L. Galichet, and K. Straif, "Carcinogenicity of radiofrequency electromagnetic fields," *The Lancet Oncology*, vol. 12, no. 7, pp. 624–626, 2011.
- [12] M. Barbiroli, C. Carciofi, V. Degli-Esposti, and G. Falciasecca, "Evaluation of exposure levels generated by cellular systems: methodology and results," *IEEE Transactions on Vehicular Technology*, vol. 51, no. 6, pp. 1322 – 1329, Nov. 2002.
- [13] Integrated Environmental Health Impact Assessment System, "EMF Path Loss Models," Tech. Rep., http://www.integrated-assessment.eu/guidebook/emf_path_loss_models.
- [14] J. Wiart, C. Dale, A. Bosisio, and A. Le Cornec, "Analysis of the influence of the power control and discontinuous transmission on RF exposure with GSM mobile phones," *IEEE Transactions on Electromagnetic Compatibility*, vol. 42, no. 4, pp. 376 –385, Nov. 2000.
- [15] T. Sarkar, Z. Ji, K. Kim, A. Medouri, and M. Salazar-Palma, "A survey of various propagation models for mobile communication," *IEEE Antennas and Propagation Magazine*, vol. 45, no. 3, pp. 51 – 82, Jun. 2003.
- [16] V. Abhayawardhana, I. Wassell, D. Crosby, M. Sellars, and M. Brown, "Comparison of empirical propagation path loss models for fixed wireless access systems," in *IEEE 61st Vehicular Technology Conference (VTC)*, vol. 1, May 2005, pp. 73 – 77.
- [17] S. Alexander, "Characterising buildings for propagation at 900 MHz," *Electronics Letters*, vol. 19, no. 20, p. 860, 1983.
- [18] M. Feuerstein, K. Blackard, T. Rappaport, S. Seidel, and H. Xia, "Path loss, delay spread, and outage models as functions of antenna height for microcellular system design," *IEEE Transactions on Vehicular Technology*, vol. 43, no. 3, pp. 487–498, Aug. 1994.
- [19] COST Action 231, "COST Action 231, Digital Mobile Radio Towards Future Generation Systems, (Final Report)," Office for Official Publications of the European Communities, Tech. Rep., 1999.
- [20] D. Moltdar, "Review on radio propagation into and within buildings," *IEE Proceedings on Microwaves, Antennas and Propagation*, vol. 138, no. 1, pp. 61 – 73, Feb. 1991.
- [21] M. Martnez-Brdalo, A. Martn, A. Sanchis, and R. Villar, "FDTD assessment of human exposure to electromagnetic fields

- from WiFi and bluetooth devices in some operating situations,” *Bioelectromagnetics*, vol. 30, no. 2, pp. 142–151, 2009. [Online]. Available: <http://dx.doi.org/10.1002/bem.20455>
- [22] A. Ahlbom, U. Bergqvist, J. H. Bernhardt, J. Cesarini, L. A. Court, M. Grandolfo, M. Hietanen, A. F. Mckinlay, M. H. Repacholi, D. H. Sliney, J. A. J. Stolwijk, M. L. Swicord, L. D. Szabo, M. Taki, T. S. Tenforde, H. P. Jammet, and R. Matthes, “Guidelines for limiting exposure to time-varying electric, magnetic, and electromagnetic fields (up to 300 GHz). International Commission on Non-Ionizing Radiation Protection.” *Health Phys*, vol. 74, no. 4, pp. 494–522, Apr. 1998. [Online]. Available: <http://view.ncbi.nlm.nih.gov/pubmed/9525427>
- [23] 3GPP TS 25.101 V10.0.1, “Universal Mobile Telecommunications System (UMTS); User Equipment (UE) radio transmission and reception (FDD),” European Telecommunications Standards Institute, Tech. Rep., May 2011.
- [24] 3GPP TS 125.104 V10.1.0, “Universal Mobile Telecommunications System (UMTS); Base Station radio transmission and reception (FDD),” European Telecommunications Standards Institute, Tech. Rep., May 2011.
- [25] K. Gilhousen, I. Jacobs, R. Padovani, A. Viterbi, J. Weaver, L.A., and I. Wheatley, C.E., “On the capacity of a cellular CDMA system,” *IEEE Trans. Vehicular Technology*, vol. 40, no. 2, pp. 303–312, May 1991.
- [26] M. Baker and T. Mouslsley, “Power control in UMTS Release ‘99,” in *1st Int. Conf. on 3G Mobile Communication Technologies (IC3G)*, 2000, pp. 36–40.
- [27] J. Kurjenniemi, S. Hamalainen, and T. Ristaniemi, “Uplink power control in UTRA TDD,” in *IEEE Int. Conf. on Communications (ICC)*, vol. 5, 2001, pp. 1522–1527.
- [28] 3GPP TS 125.331 V10.3.1, “Universal Mobile Telecommunications System (UMTS); Radio Resource Control (RRC); Protocol specification,” European Telecommunications Standards Institute, Tech. Rep., May 2011.
- [29] “Bridge Ratings Industry Study: In-Car Cell Phone Use,” Bridge Ratings, LLC, Tech. Rep., Feb. 2006.
- [30] A. Lenhart, “Cell phones and American adults,” Pew Research Center, Tech. Rep., Sep. 2010.
- [31] “Network Interface Publication,” Vodafone Ireland, Tech. Rep., 2009.
- [32] S. Su, *The UMTS air-interface in RF engineering: design and operation of UMTS networks*. McGraw-Hill, 2007. [Online]. Available: <http://books.google.com/books?id=0V50yMZi9F8C>
- [33] “Mobile Sites; Base Stations and Masts,” ComReg, Tech. Rep., Aug. 2011, http://www.askcomreg.ie/mobile/View_Mobile_Sites.36.LE.asp.